



New *flow* S3 Mid-Power Package – the Smarter Way

The new baseplate-less *flow* S3 package extends the power range of Vincotech's well established *flow* housing family. The housing is tailored for applications demanding more power in small footprint for example solar inverters or motor drives.

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Introduction

Engineers aim for higher power ratings, increased power density and, ultimately, more power in the same frame size. An increase of ceramic substrate size to accommodate the required semiconductors for higher power rating, while keeping a small package foot print, is the key. The sweet spot comes by lack of a copper baseplate and by lack of system solder, which results reduced cost and increased reliability. A new baseplate-less package with single big ceramic substrate will be introduced in this article.

***flow* S3 package description**

The new baseplate-less housing *flow* S3 comprises 67% more ceramic area than *flow* 1. The outline dimensions of *flow* 1 are increased along the two blue arrows in y-direction (Figure 1:) while keeping the screw hole distance and the dimensions in x-direction. Beside the dimensional increase the thermal performance was in special focus during *flow* S3 design. The ceramic substrate thickness is reduced and the contact pressure between ceramic and heat sink is increased. The *flow* S3 housing lacks a heavy copper baseplate which makes it a very affordable module.

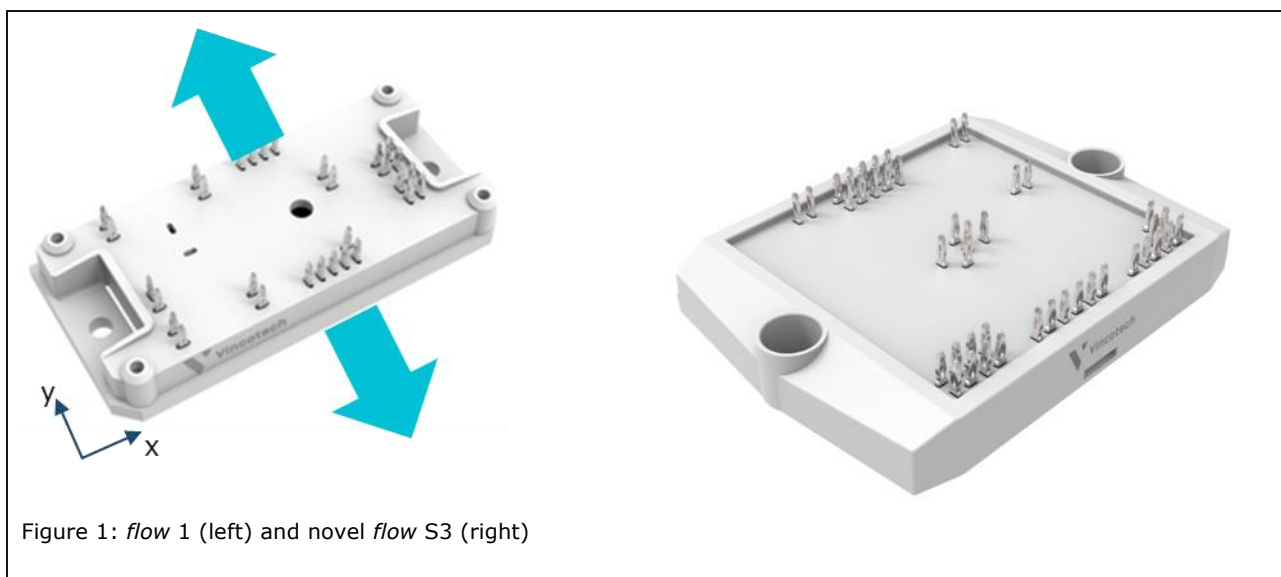


Figure 1: *flow 1* (left) and novel *flow S3* (right)

With the benefit of their low stray inductance, the 12 mm housing prominently features applications where fast switching speed and high efficiency are needed. Low inductivity is also supported by the free placement of pins and the possibility to integrate ceramic capacitors, resulting in low voltage overshoot. Plastic housing material with comparative tracking index of 600 (CTI600) makes the *flow S3* housing the best choice for 1500 V applications.

The inside technology of *flow S3* increases the ruggedness of the single big ceramic substrate during the mounting process of the module. Press-fit pins and pre-applied phase-change material further support fast and easy assembly at the customer side.

Pressure distribution and thermal resistance

High thermal performance is equivalent to a low thermal resistance $R_{th(j-s)}$ from the semiconductor junction to the heat sink, which is the key for higher power density. An improvement in the thermal resistance can be obtained by optimizing the two main contributors on the thermal resistance: ceramic substrate and thermal interface material (TIM). Especially for the latter the pressure or contact force on the interface is influencing the thermal resistance.

Figure 2 shows the pressure distribution between DCB and heat sink of *flow S3* and a competitor package. The novel baseplate-less package *flow S3* appears with overall higher contact pressure and more uniform pressure distribution.

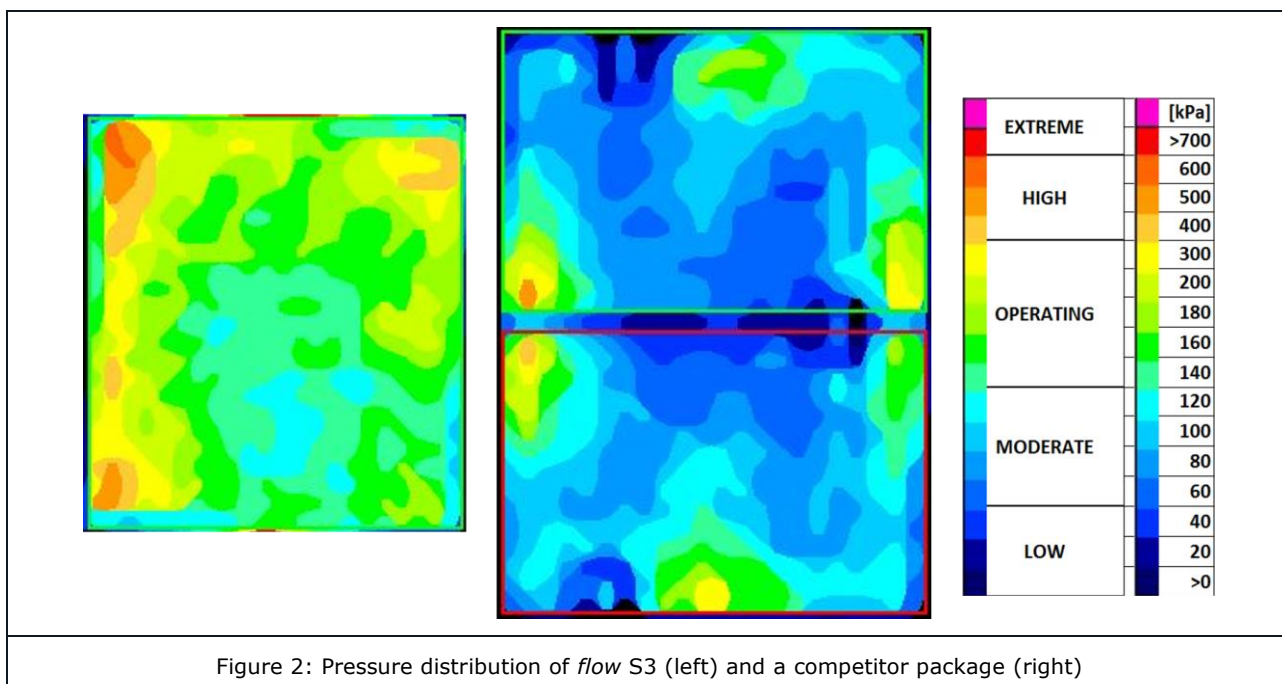


Figure 2: Pressure distribution of *flow S3* (left) and a competitor package (right)

The pressure distribution is only the first indicator for better thermal performance. The proof is furnished by the measurement of the thermal resistance $R_{th(j-s)}$ between the semiconductor junction and the heat sink (Figure 3). The thermal resistance of *flow S3* is 16% lower than Vincotech standard technology.

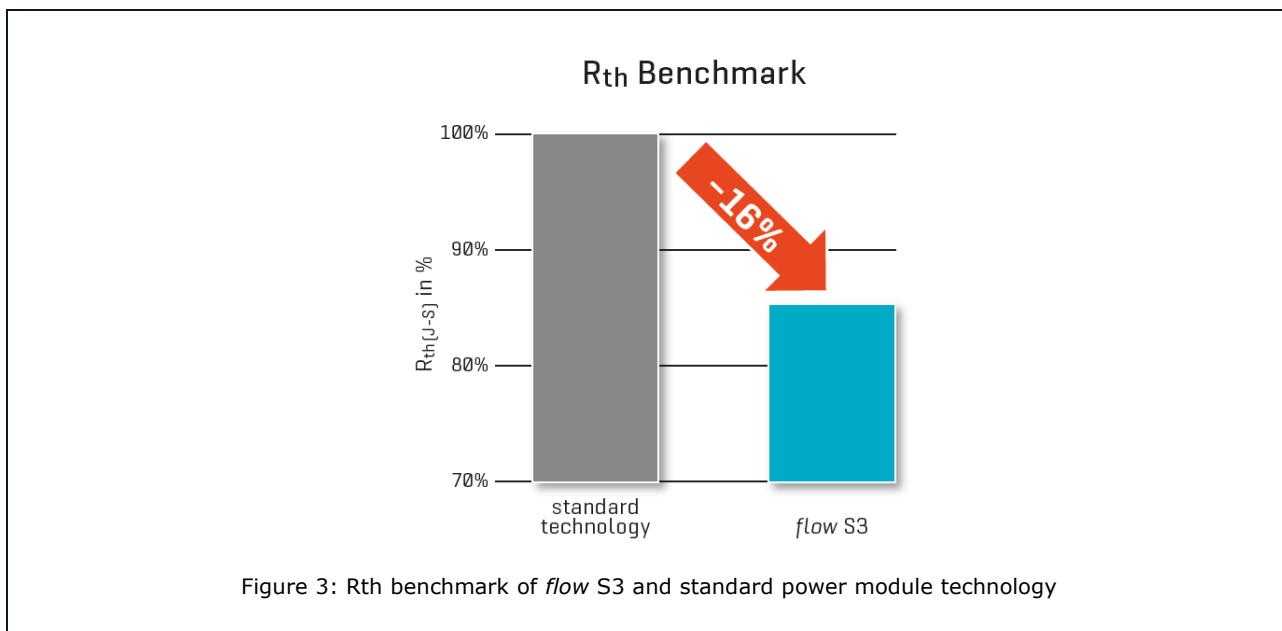


Figure 3: R_{th} benchmark of *flow S3* and standard power module technology

The consequence of smaller thermal resistance is a lower chip junction temperature at the same output power and, thus, longer lifetime. At the same junction temperature the housing with the lower thermal resistance can deliver higher output power.



Validation of no TIM pump-out

The pump-out of the thermal interface material (TIM) is well known from baseplate modules. The root cause of TIM pump-out is thermo-mechanical movement of the baseplate at changing temperatures. The temperature change can be active by increase or decrease of the power or passive by change of ambient temperature. In both cases the thermo-mechanical movement of the baseplate pushes the TIM material to the edges of the baseplate.

Since *flow S3* is a baseplate-less package, no pump-out can be observed at active or passive cycling. The former is checked by long power cycling (PC minutes) test and the latter by a passive thermal cycling (TC) test.

Figure 4 shows the trend of the thermal resistance (R_{th}) junction to heat sink of *flow S3* over 54k cycles of a power cycling minutes test. During the first cycles the phase change material melts and distributes homogenously. After this event the R_{th} stabilizes and stays constant for the rest of the cycles. Failure criteria for this test is an increase of R_{th} by 20% referenced to the initial value. The test was stopped without failure after 54k cycles.

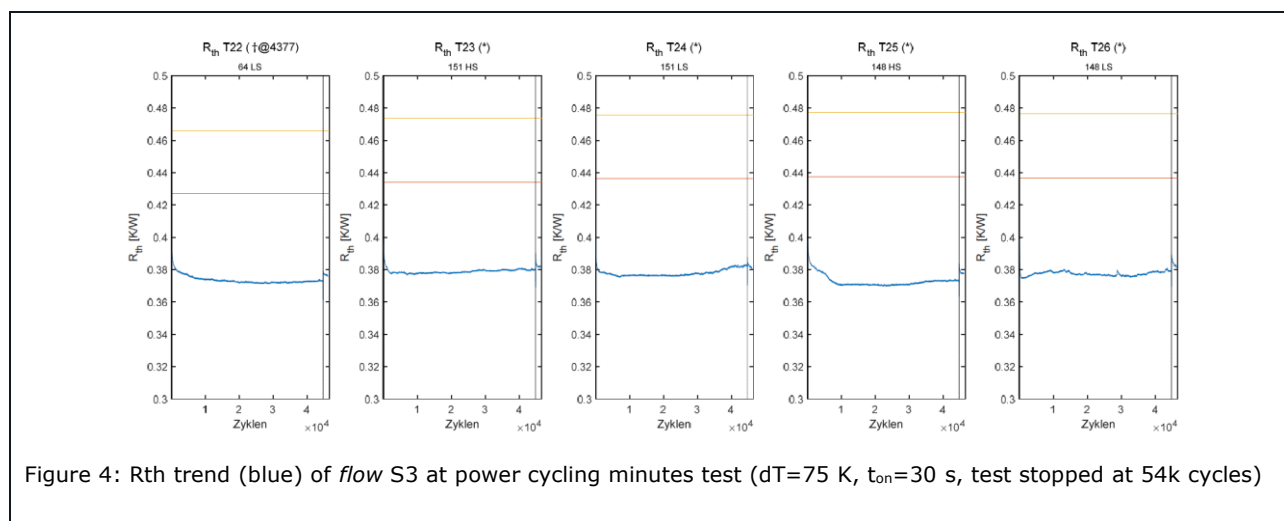


Figure 5 shows the normalized thermal resistance trend of *flow S3* at passive thermal cycling from -40 °C to +125 °C with 30 minutes dwell time at each temperature. The test aperture has two chambers and the mounted modules are moved from one chamber to the other within less than 1 minute. This test is also known as temperature shock. Failure criteria for the passive thermal cycling test is an R_{th} increase by 20% referenced to the initial value.

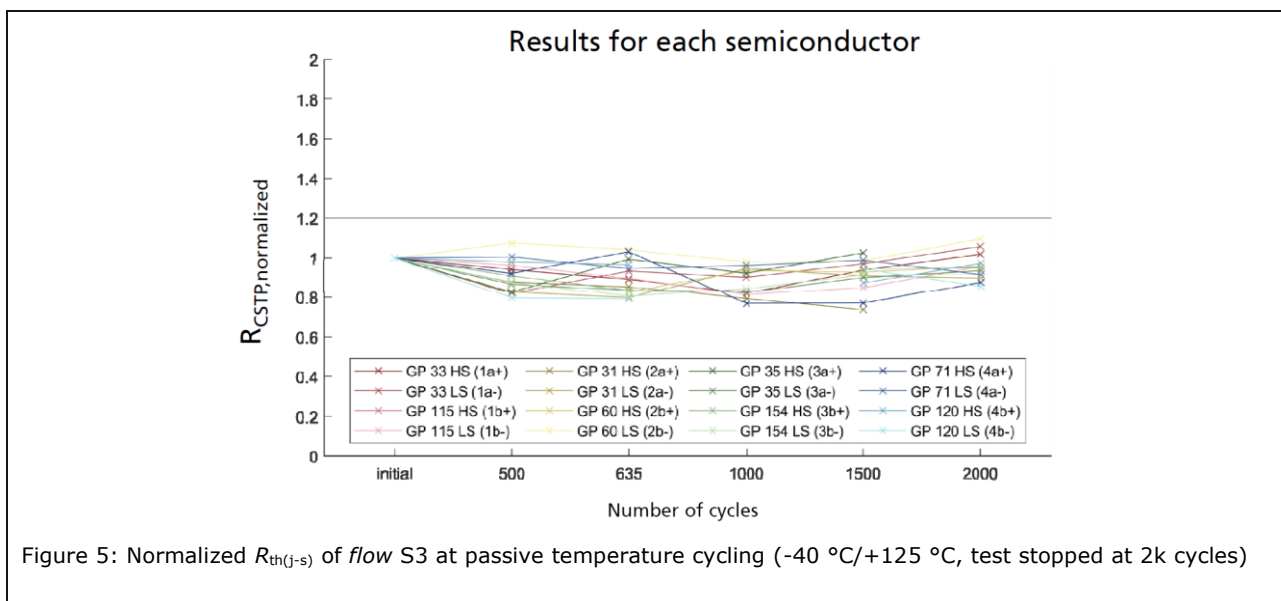
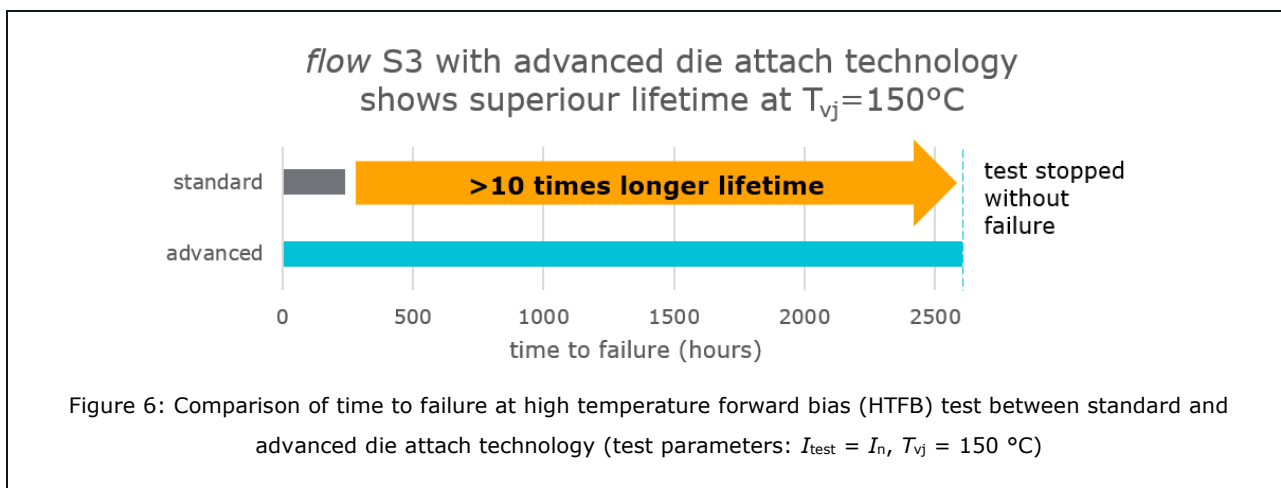


Figure 5: Normalized $R_{th(j-s)}$ of flow S3 at passive temperature cycling (-40 °C/+125 °C, test stopped at 2k cycles)

From the test results it can be concluded that the thermal resistance of flow S3 is long-term stable. Neither power cycling minutes nor passive temperature cycling, are able to trigger TIM pump-out, which would be indicated by an increase of thermal resistance.

Superior die attach technology for increased lifetime

For validation of the long term reliability of the solder joint a highly accelerated High Temperature Forward Bias (HTFB) test is carried out. The HTFB test is performed at nominal chip current and maximum operation junction temperature. Failure mode is delamination of the solder joint, which yields to increase of the thermal resistance. The failure criteria is an increase of the thermal resistance by 20%. After 2700 hours the test was stopped without failure of the advanced die attach technology. The advanced die attach technology shows more than 10 times longer lifetime (Figure 6) than standard technology.

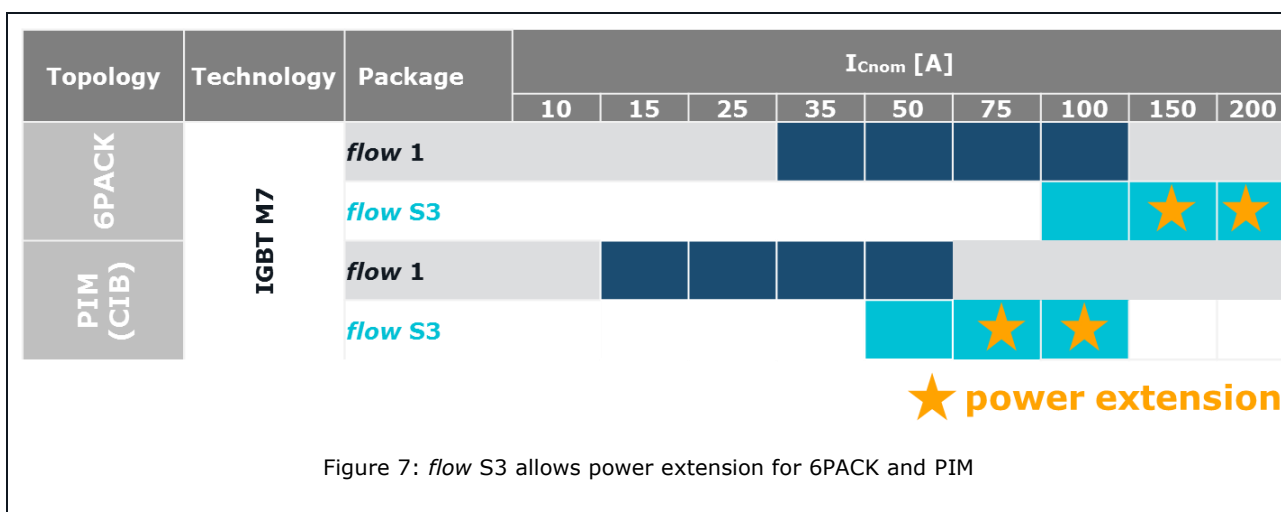


Applications with mission profiles containing long operation time at high temperatures together with high current benefit directly from the lifetime increase of the advanced solder technology. Those applications are for instance solar inverters with an oversized solar generator.

Application examples

In 1500 V multi-string solar applications the *flow S3* housing supports inverter output power beyond 300 kW and fosters the trend to further increase the inverter output power and power density.

For motor drive applications the combination of more ceramic area and lower thermal resistance allows the doubling of the maximum nominal current of 6PACK and PIM configuration in *flow S3* to 200 A respectively 100 A (Figure 7). The module power density (kW/cm^2) can be increased up to 12% with *flow S3*.





Conclusion

This article introduces the new *flow* S3 baseplate-less medium power package and highlights the superior thermal performance achieved by high and uniform pressure distribution. The long term stability of R_{th} is proven by the active power cycling and passive temperature cycling tests. High reliability is also supported by the lifetime increase introduced with the advanced die attach technology. In summary, the *flow* S3 housing is the perfect fit for all applications demanding high power in small footprint.